



COST Action E55

Timber Structures exposed to Moisture

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Problem overview

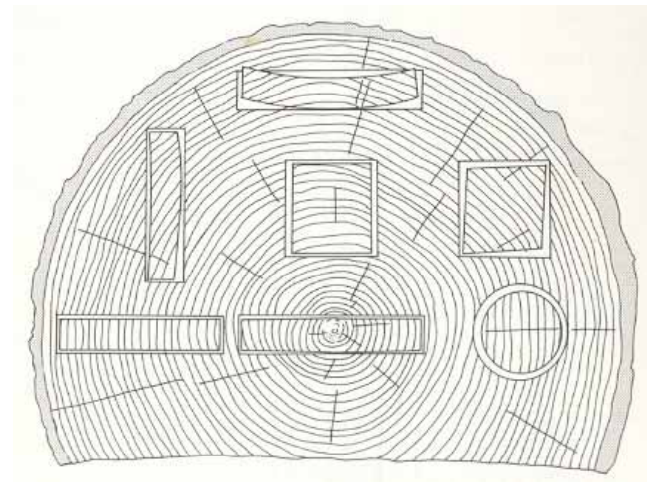
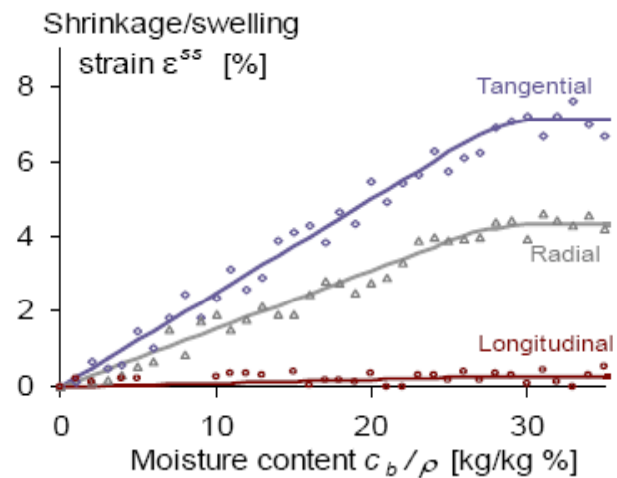
- The load bearing capacity of timber structural elements is affected by moisture and moisture variations, and, time history of applied loading (duration of load effect)
- In design codes, as e.g. the EC, these effects are accounted for by a factorization of strength with a modification factor (k_{mod})

Material	Standard	Service class	Load-duration class				
			Permanent action	Long term action	Medium term action	Short term action	Instantaneous action
Solid timber	EN 14081-1	1	0,60	0,70	0,80	0,90	1,10
		2	0,60	0,70	0,80	0,90	1,10
		3	0,50	0,55	0,65	0,70	0,90
Glued laminated timber	EN 14080	1	0,60	0,70	0,80	0,90	1,10
		2	0,60	0,70	0,80	0,90	1,10
		3	0,50	0,55	0,65	0,70	0,90

Problem overview (cont.)

- The effect of moisture on the load bearing behaviour might be differentiated:

- Stresses due to restrained shrinkage and swelling of the timber

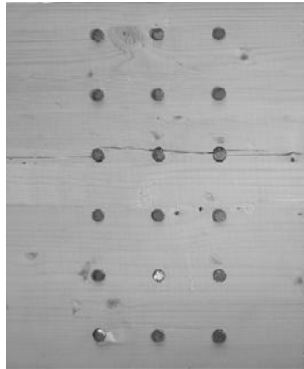


- Accelerated aging (+DOL) as a result of moisture state and history

Problem overview (cont.)

- The effect of moisture on the load bearing behaviour might be differentiated:
 - Stresses due to restrained shrinkage and swelling of the timber

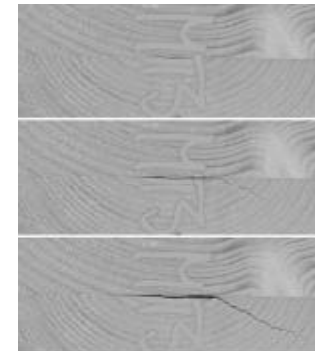
Connections



Drying



Wetting

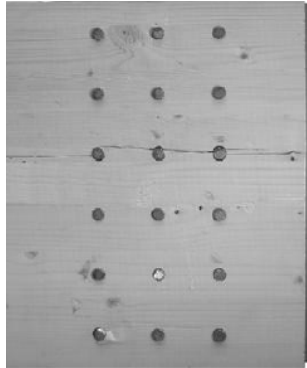


- Accelerated aging (+DOL) as a result of moisture state and history

Problem overview (cont.)

- The effect of moisture on the load bearing behaviour might be differentiated:
 - Stresses due to restrained shrinkage and swelling of the timber [Type I]

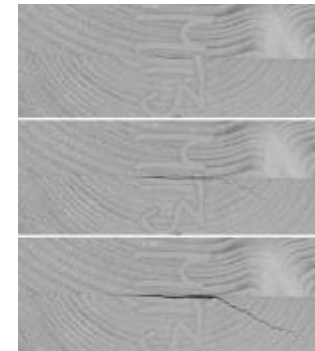
Connections [Ia]



Drying [Ib]



Wetting [Ib]



- Accelerated aging (+DOL) as a result of moisture state and history [Type II]

Problem overview (cont.)

- Moisture effects as a problem when structures had failed:

Failure Mode	% of cases analysed	Moisture Influence
Instability	30	Likely (deformations)
Bending failure	15	Possible (aging)
Tension failure perp.	11	Yes, MIS
Shear failure	9	Likely (cracks)
Drying cracks	9	Yes
Excessive deflection	7	Yes (creep)
Tension failure	5	Possible (aging)
Corrosion of fasteners / decay	4	Yes
Withdrawal of fasteners	3	Possible
Compression	2	Possible
Other / unknown	21	-

Problem overview (cont.)

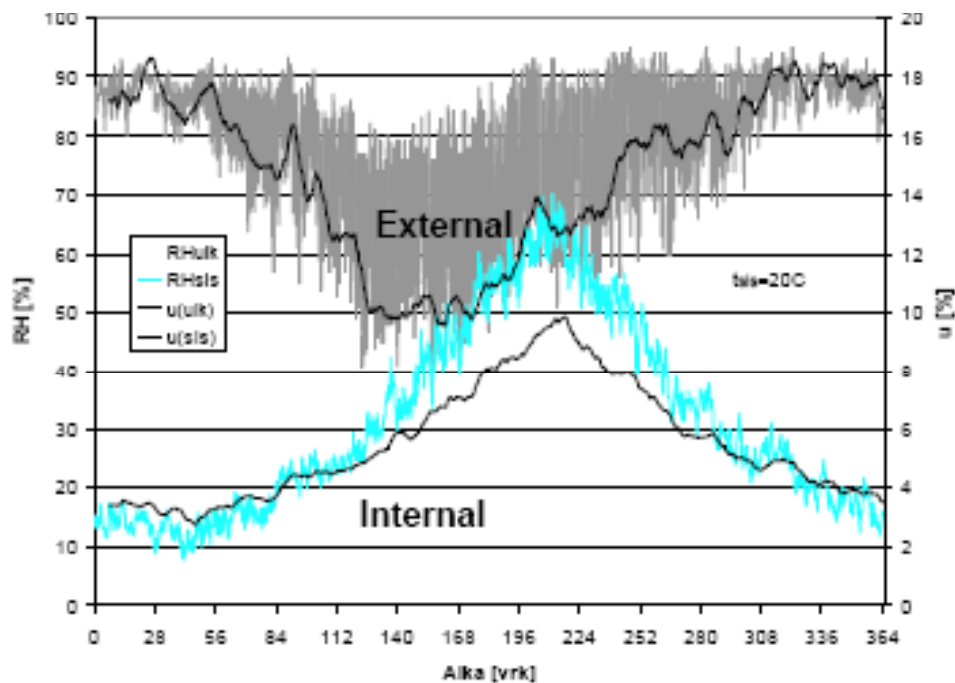
- Problem character and possible measures:

Effect	Characteristics	Design measures
I a – rest. shrink. connections	-Moisture induced stresses. -Stress dependent on peak to peak amplitude, period of RH and comp. cross section.	-Specific regulations on: + Dowel arrangement perp. grain + initial moisture contents + in-service moisture contents
I b - rest. shrink. cross sections	-RH history not of interest – time independent.	- Moisture stress design for key components.
II - aging	- reduced strength - Combined effect of load and RH history – time dependent.	- k_{mod} principle seems o.k. - further development of model basis necessary. -Refinement of load duration and climate classification in codes.

Indoor and outdoor climate

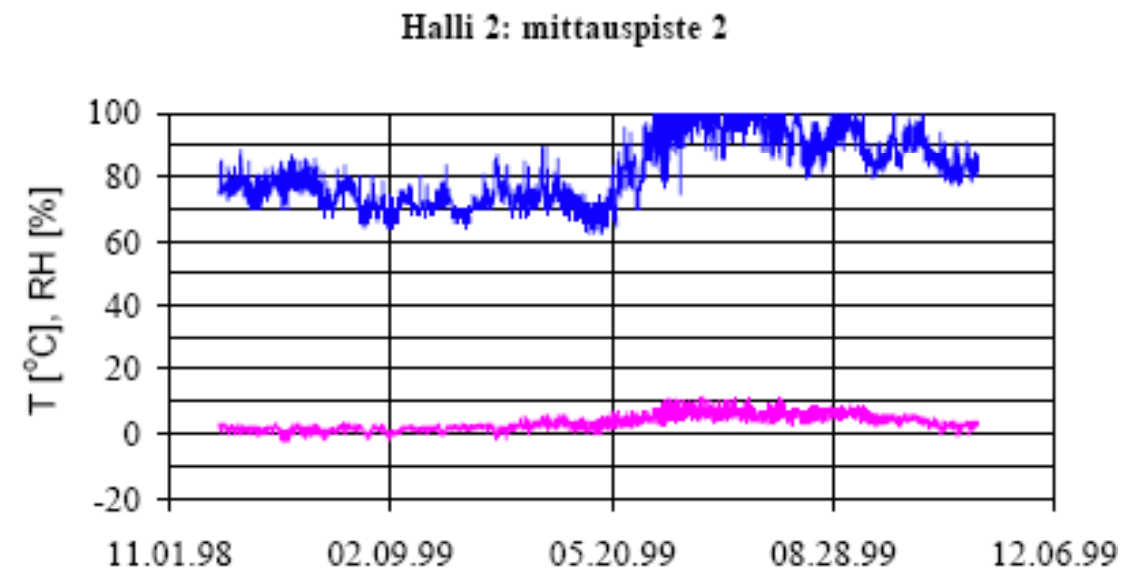
- Example:

Sibelius hall



Ref: Koponen, 2002

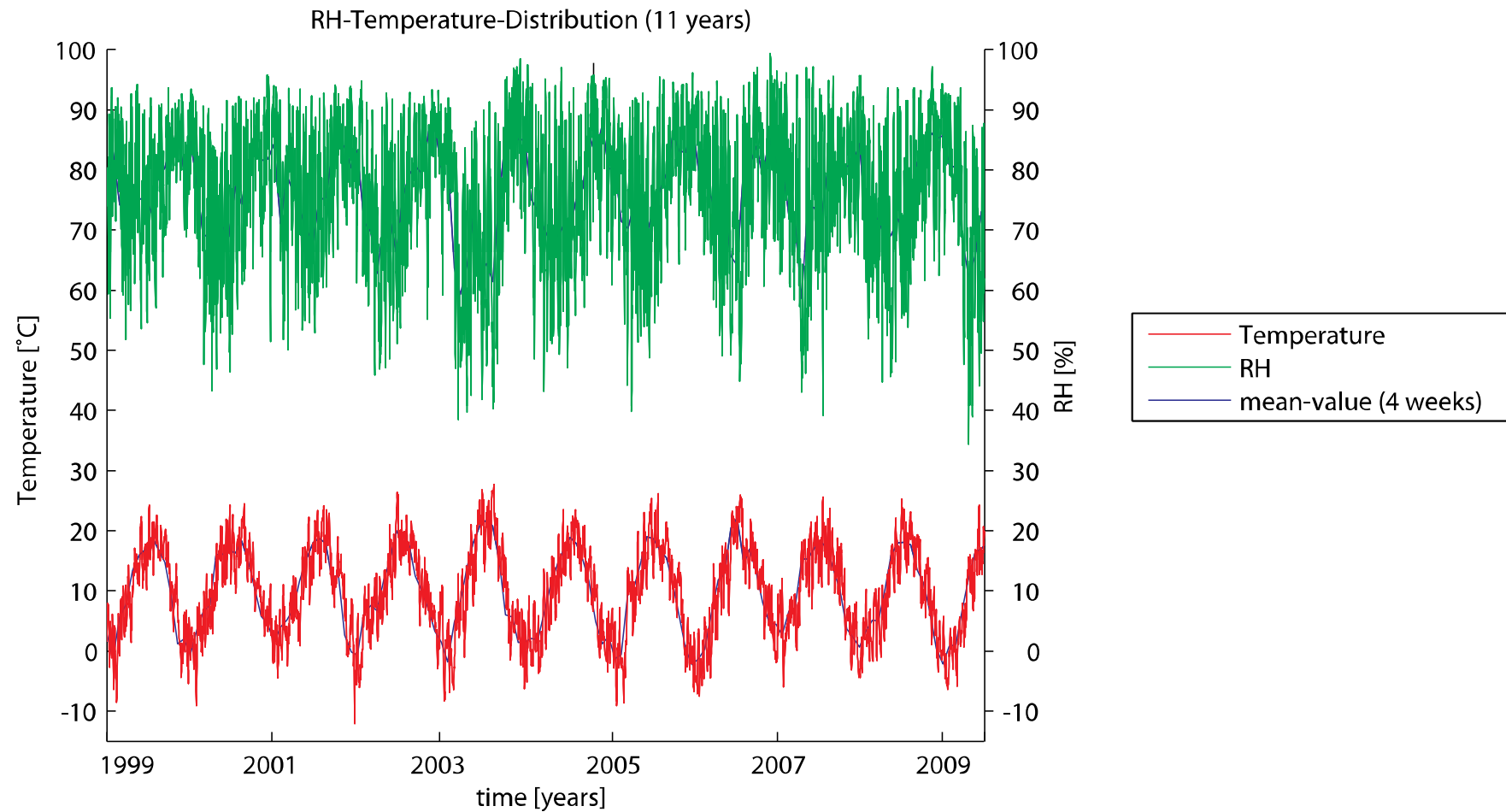
Ice skating hall



Ref: Kevarinmäki et al., 2000

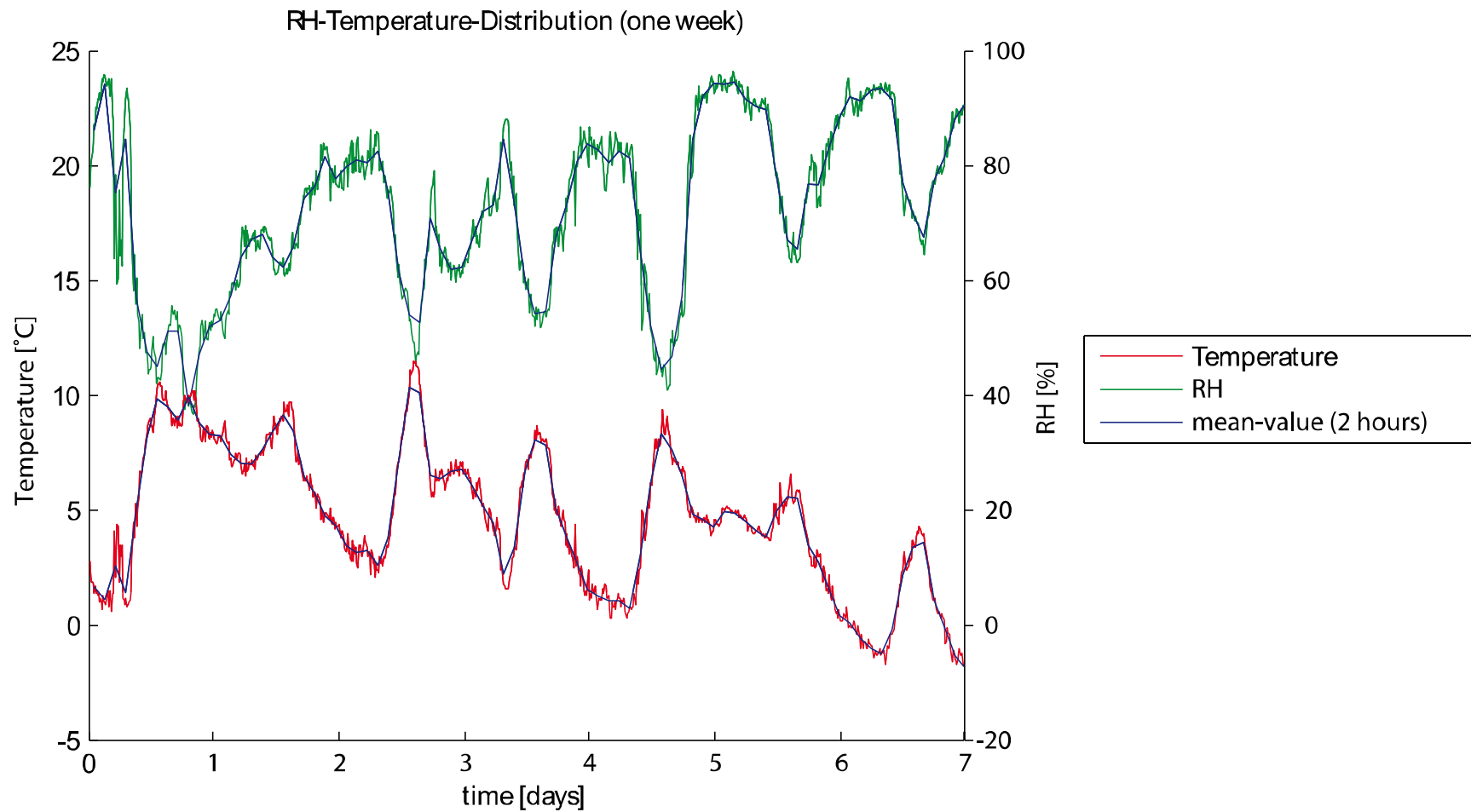
Indoor and outdoor climate

- Example:



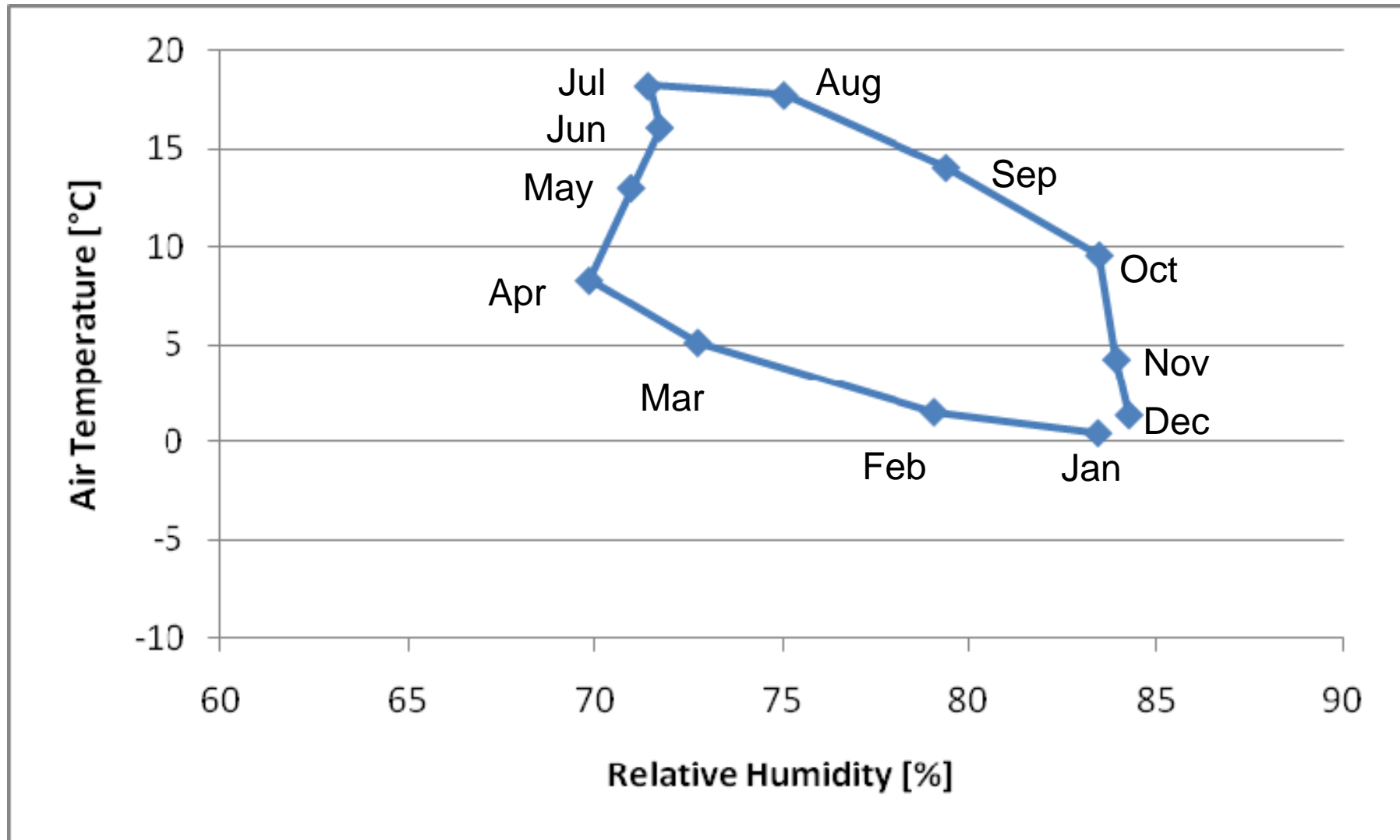
Indoor and outdoor climate

- Example:



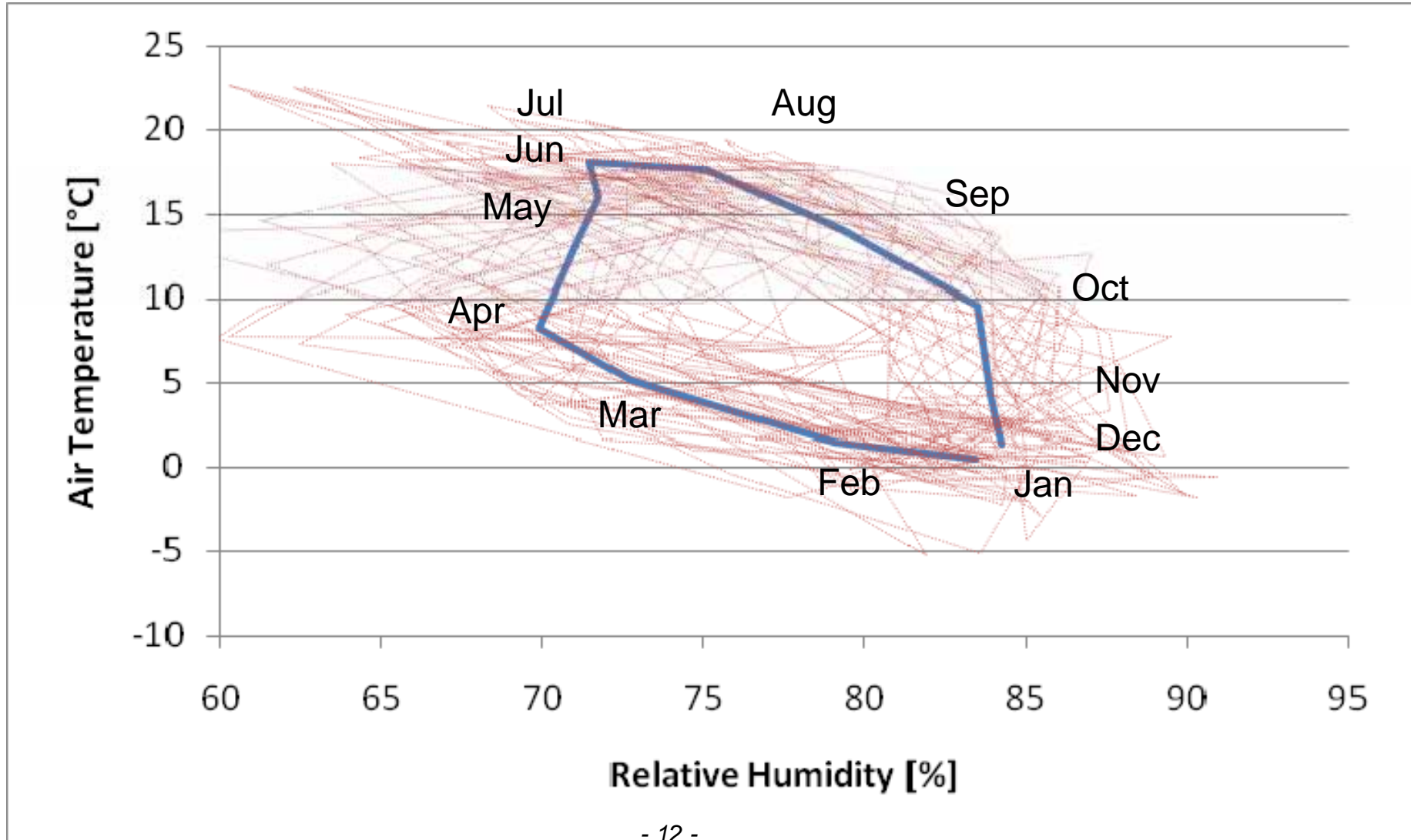
Indoor and outdoor climate

- Example:



Indoor and outdoor climate

- Example:



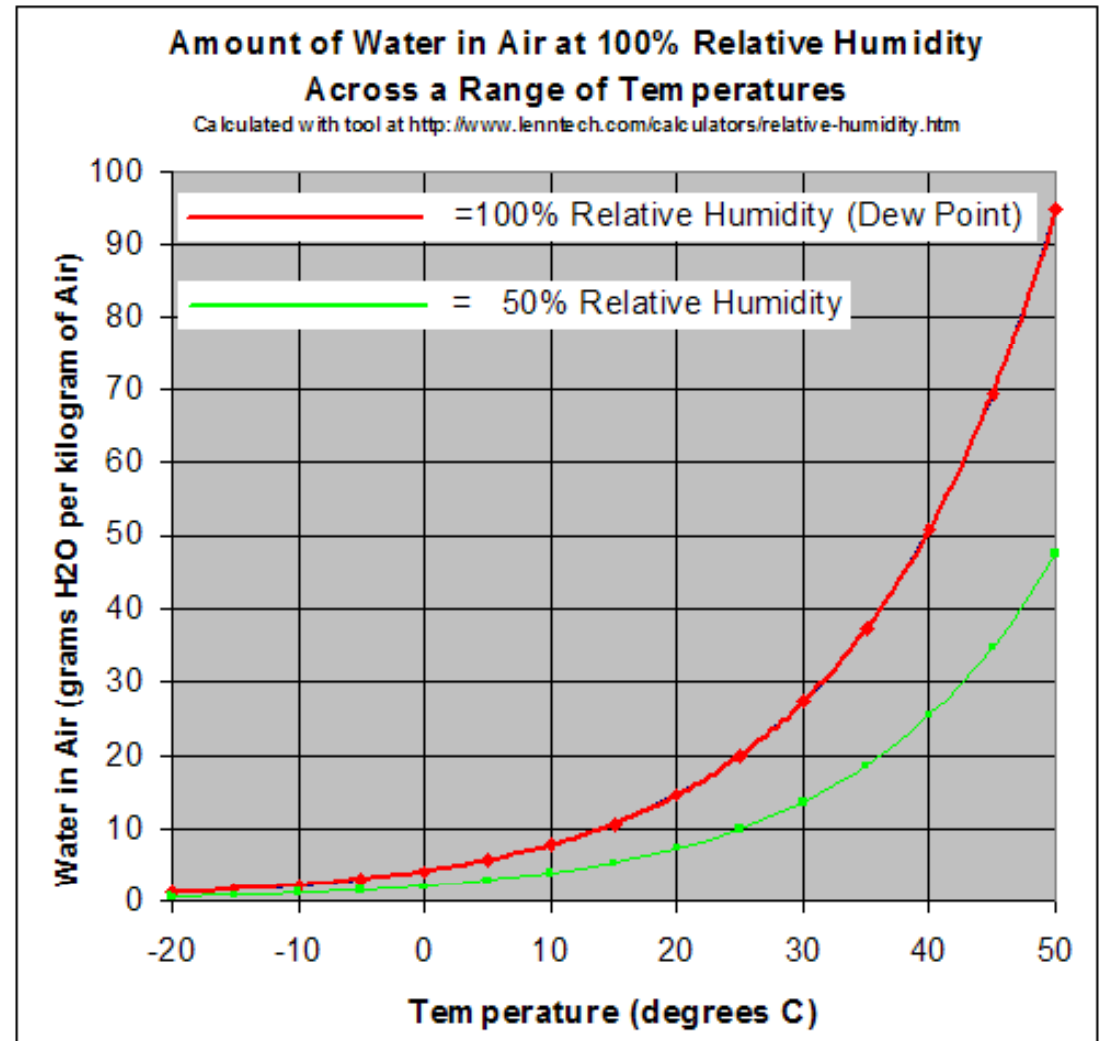
Indoor and outdoor climate

- Good empirical basis for outside climates.
- Approach: Modelling the indoor climate as a function of:
 - The outdoor climate
 - Indoor moisture and heat production
 - Ventilation.

Building climate relations

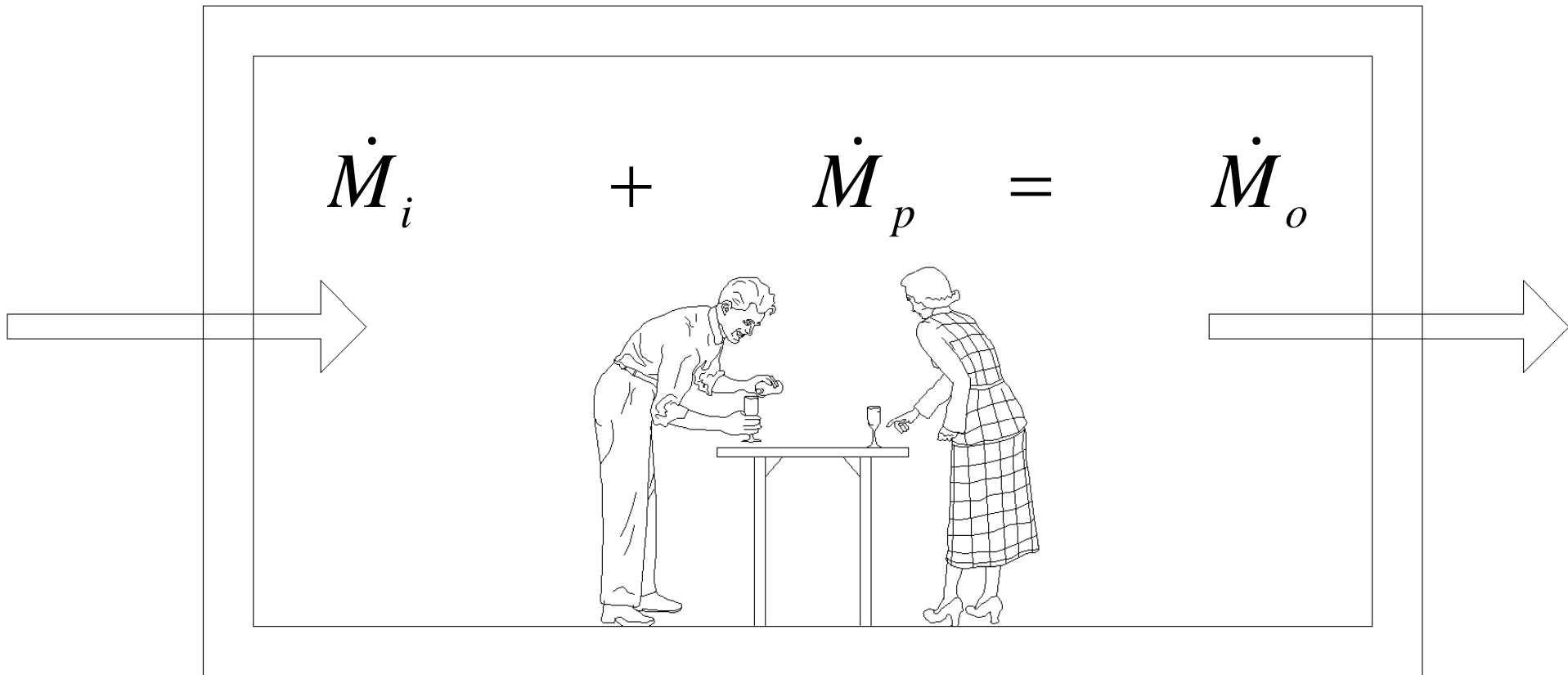
- Satiation level depends on the temperature
- Relative Humidity:

$$\varphi = \frac{c}{c_s} = \frac{\text{vapor content}}{\text{max vapor content}}$$



Building climate relations

- Humidity equilibrium



Building climate relations

- Humidity equilibrium

$$\dot{M}_i + \dot{M}_p = \dot{M}_o$$

$$L \cdot V \cdot \varphi_o \cdot c_{so} \cdot \frac{T_o}{T_i} + \dot{M}_p = L \cdot V \cdot \varphi_i \cdot c_{si}$$

L Air alteration rate [h^{-1}]

V Volume [m^3]

$\varphi_{o,i}$ Relative Humidity (outside/inside)

$c_{so,si}$ Satiation vapor content

$T_{o,i}$ Temperature

Building climate relations

- Humidity equilibrium

$$\varphi_i = \varphi_o \frac{c_{so}}{c_{si}} \cdot \frac{T_o}{T_i} + \frac{M_p}{L \cdot V \cdot c_{si}}$$

L Air alteration rate [h^{-1}]

$c_{so,si}$ Satiation vapor content

V Volume [m^3]

$T_{o,i}$ Temperature

$\varphi_{o,i}$ Relative Humidity (outside/inside)

Building climate relations

- Humidity equilibrium

$$L = \infty \rightarrow \varphi_i \cdot c_{si} \cdot T_i = \varphi_o \cdot c_{so} \cdot T_o$$

Vapor content inside = Vapor content outside

L Air alteration rate [h^{-1}]

$c_{so,si}$ Satiation vapor content

V Volume [m^3]

$T_{o,i}$ Temperature

$\varphi_{o,i}$ Relative Humidity (outside/inside)

Building climate relations

- Reference Values:

– Produced Humidity	M_p [g / h]
Office working person	50
handcrafter	150
Professional athlete	1000
cooking	500 – 1000
- Air alteration rate	L [h^{-1}]
Tilted window + down shutters	0.3 – 1.5
Tilted window	0.8 – 2.5
Tilted window + cross-ventilation	2.0 – 4.0
Half-open window	5.0 – 10.0
Open window	9.0 – 15.0
Open window + cross-ventilation	20.0 – 40.0

Building climate relations

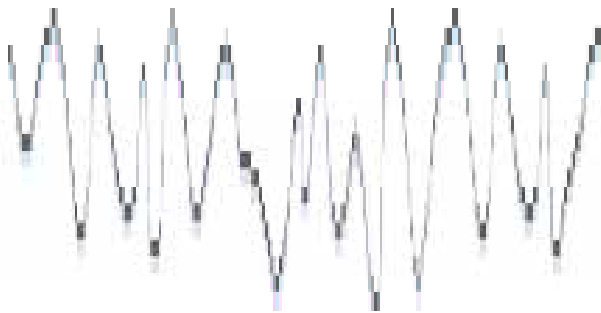
- Reference Values:

– Building Types	φ_i [%] (yearly cycle)
Outdoor sheltered	100 - 55
Indoor heated	15 - 60
Swimming, Ice skating	75 - 99
Hospitals	40 – 60
Theater, Sports	50 – 80
Stair case	50 – 70
Industry	40 - 50

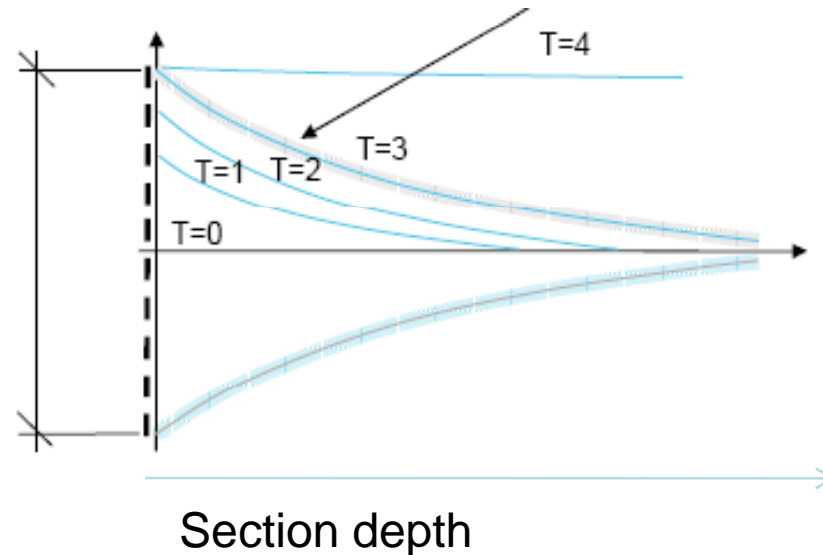
Summary and Outlook

- Highly resolved outdoor climate data available
- Indoor climate as a function of outdoor climate and building characteristics
- Proper time resolution of the data?

RH (amp, frequency)



Moisture content amplitude



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Thank you for
your attention

